

APPENDIX C: TOTAL EXPOSURE RATIO

FCC ID: A3LSMF936U	NEAR-FIELD POWER DENSITY EVALUATION REPORT	Approved by: Technical Manager
DUT Type: Portable Handset		APPENDIX C: Page 1 of 9



The Total Exposure Ratio (TER) is calculated by combining all SAR measurements and power density measurements after normalizing to their respective limits. The general expression is below.

$$TER = \sum_{a=1}^{A} \frac{SAR_a}{SAR_a, limit} + \sum_{b=1}^{B} \frac{psPD_b}{psPD_b, limit} < 1$$

The TER shall be less than unity to ensure compliance with the limits.

$$\sum_{n=1}^{N} \frac{4G \ SAR_n}{4G \ SAR_n, limit} + \sum_{m=1}^{M} \frac{5G \ mmW \ NR \ psPD_m}{5G \ mmW \ NR \ psPD_m, limit} + \sum_{p=1}^{P} \frac{WLAN \ SAR_p}{WLAN \ SAR_p, limit} < 1$$

Qualcomm® Smart Transmit algorithm for WWAN adds directly the time-averaged RF exposure from 4G and time-averaged RFexposure from 5G mmW NR. Smart Transmit algorithm controls the total RF exposure from both 4G and 5G mmW NR to not exceed FCC limit. Therefore, per FCC guidance, TER does not need to be evaluated directly for the 4G and 5G simultaneous compliance via summation. The following equations are derived later in Appendix C. The validation of the time-averaging algorithm and compliance under the Tx varying transmission scenario for WWAN technologies are reported in Part 2 report. The report SN could be found in Bibliography section.

$$\sum_{n=1}^{N} \frac{4G SAR_n}{4G SAR_n, limit} + \sum_{p=1}^{P} \frac{WLAN SAR_p}{WLAN SAR_p, limit} < 1$$

$$\sum_{m=1}^{M} \frac{5G \ mmW \ NR \ psPD_{m}}{5G \ mmW \ NR \ psPD_{m}, limit} + \sum_{p=1}^{P} \frac{WLAN \ SAR_{p}}{WLAN \ SAR_{p}, limit} < 1$$

For 5G mmW NR, since there is total design-related uncertainty arising from TxAGC and device-to-device variation, the worst-case RF exposure should be determined by accounting for device uncertainty. For this device, the manufacturer has added an additional permanent back-off (indicated below as WWAN backoff) for every beam in the calculations for input.power.limits used in the EFS file. The back-off levels can be found in the Part 0 Test report. Therefore, 5G mmW NR RF exposure for this DUT is evaluated by reported psPD calculated as:

Note that since not all the beams supported by this EUT are measured, reported_psPD cannot be computed based on limited measured psPD data. Alternatively, since measured psPD for all the beams will be ≤ PD_design_target + PD_uncertainty uncertainty, reported_psPD is computed based on this worst-case psPD as shown above.

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The compliance analysis for simultaneous transmission scenarios of WWAN (4G LTE & 5G mmW NR) with Smart Transmit and 4G & WLAN can be found in two reports indicated in the table below. This appendix demonstrates compliance for the 5G + WLAN scenarios. The report SNs can be found in Bibliography section.

	Simultaneous Scenario	Evaluation Report
1.	4G LTE WWAN + WLAN	FCC SAR Evaluation Report (Part 1)
2.	4G LTE WWAN + 5G mmW NR WWAN	RF Exposure Part 2 Test Report

RF exposure compliance with 5G mmW NR WWAN+WLAN simultaneous transmission scenarios is demonstrated for various radio configurations below.

Note that the above reported psPD applies to the worst-case surfaces of the DUT at 2mm evaluation distance.

Worst-case PD on other surfaces of the DUT are calculated from simulated PD data (see Power Density Simulation Report), by multiplying reported psPD with the highest proportion out of all beams and out of all three channels in each band, where the adjustment for each beam/channel is computed as the proportion of "simulated PD on desired surface" to "simulated PD on worst-surface". For example, to determine worst-case PD on front surface (needed for Head RF Exposure evaluation during simultaneous transmission), highest proportion of (simulated PD on front surface)/(simulated PD on worst surface) was determined out of all supported beams and out of all three channels by the DUT in each band.

In some cases, the simulation vs measurement for some surfaces can exceed the device's total uncertainty. In those cases, if the measured psPD > simulated adjusted psPD (assuming a linear congruency of the psPD across surfaces), then measured psPD should be used towards the simultaneous TX analysis. Table C-1 lists the relevant worst-case reported psPD values based on the additional surfaces and evaluation distances needed to perform the TER analysis. The highest of the adjusted Reported_psPD and Measured Total psPD was chosen for TER analysis and the chosen values are indicated by bolded psPD values.

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Table C-1 5G mmW NR FR2 psPD - Closed

NR Band				<u> </u>	TIVE POLID	10300		
n258 J Front 2 0.041 0.030 0.206 0.206 n258 J Top 2 0.145 0.107 - 0.107 n258 J Bottom 2 0.114 0.084 - 0.084 n258 J Right 2 0.108 0.080 - 0.080 n258 J Left 2 0.735 0.545 0.073 0.545 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000	NR Band	Antenna	<u>Surface</u>		Factor due to	Reported psPD		Final Reported psPD (mW/cm²)
n258 J Top 2 0.145 0.107 - 0.107 n258 J Bottom 2 0.114 0.084 - 0.084 n258 J Right 2 0.108 0.080 - 0.080 n258 J Left 2 0.735 0.545 0.073 0.545 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.676	n258	J	Back	2	1.000	0.741	0.373	0.741
n258 J Bottom 2 0.114 0.084 - 0.084 n258 J Right 2 0.108 0.080 - 0.080 n258 J Left 2 0.735 0.545 0.073 0.545 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Front 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 <t< td=""><td>n258</td><td>J</td><td>Front</td><td>2</td><td>0.041</td><td>0.030</td><td>0.206</td><td>0.206</td></t<>	n258	J	Front	2	0.041	0.030	0.206	0.206
n258 J Right 2 0.108 0.080 - 0.080 n258 J Left 2 0.735 0.545 0.073 0.545 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.676 0.524 0.759 n261 J Back 2 1.000	n258	J	Тор	2	0.145	0.107	-	0.107
n258 J Left 2 0.735 0.545 0.073 0.545 n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Top 2 0.031 <	n258	J	Bottom	2	0.114	0.084	-	0.084
n258 K Back 2 1.000 0.676 0.320 0.676 n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Right 2 0.037 0.028 - 0.028 n261 J Right 2 0.057	n258	J	Right	2	0.108	0.080	-	0.080
n258 K Front 2 0.420 0.284 0.192 0.284 n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Front 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 K Back 2 1.003 <	n258	J	Left	2	0.735	0.545	0.073	0.545
n258 K Top 2 0.424 0.287 0.319 0.319 n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Bottom 2 0.037 0.028 - 0.079 n261 J Bottom 2 0.057 0.044 - 0.044 n261 J Right 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000	n258	K	Back	2	1.000	0.676	0.320	0.676
n258 K Bottom 2 0.046 0.031 - 0.031 n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Front 2 0.037 0.028 - 0.029 n261 J Bottom 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 <td< td=""><td>n258</td><td>К</td><td>Front</td><td>2</td><td>0.420</td><td>0.284</td><td>0.192</td><td>0.284</td></td<>	n258	К	Front	2	0.420	0.284	0.192	0.284
n258 K Right 2 1.000 0.676 0.304 0.676 n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.779 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Top 2 0.104 0.079 - 0.079 n261 J Bottom 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422	n258	K	Тор	2	0.424	0.287	0.319	0.319
n258 K Left 2 0.062 0.042 - 0.042 n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Top 2 0.104 0.079 - 0.079 n261 J Right 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.057 0.044 - 0.044 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Right 2 1.000 0.676	n258	К	Bottom	2	0.046	0.031	-	0.031
n261 J Back 2 1.000 0.759 0.524 0.759 n261 J Front 2 0.031 0.024 0.171 0.171 n261 J Top 2 0.104 0.079 - 0.079 n261 J Bottom 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Front 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000	n258	К	Right	2	1.000	0.676	0.304	0.676
Name	n258	К	Left	2	0.062	0.042	-	0.042
n261 J Top 2 0.104 0.079 - 0.079 n261 J Bottom 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Front 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000	n261	J	Back	2	1.000	0.759	0.524	0.759
n261 J Bottom 2 0.037 0.028 - 0.028 n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Front 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000	n261	J	Front	2	0.031	0.024	0.171	0.171
n261 J Right 2 0.057 0.044 - 0.044 n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032	n261	J	Тор	2	0.104	0.079	-	0.079
n261 J Left 2 0.723 0.549 0.178 0.549 n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Bottom 2 0.192	n261	J	Bottom	2	0.037	0.028	-	0.028
n261 K Back 2 1.000 0.676 0.190 0.676 n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Right 2 0.093	n261	J	Right	2	0.057	0.044	-	0.044
n261 K Front 2 0.367 0.248 0.390 0.390 n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Right 2 0.108 0.080 - 0.080 n260 J Right 2 0.672 0.4	n261	J	Left	2	0.723	0.549	0.178	0.549
n261 K Top 2 0.422 0.285 0.254 0.285 n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.6	n261	К	Back	2	1.000	0.676	0.190	0.676
n261 K Bottom 2 0.035 0.024 - 0.024 n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0	n261	К	Front	2	0.367	0.248	0.390	0.390
n261 K Right 2 1.000 0.676 0.301 0.676 n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.080 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Bottom 2 0.537 <	n261	К	Тор	2	0.422	0.285	0.254	0.285
n261 K Left 2 0.049 0.033 - 0.033 n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 <td< td=""><td>n261</td><td>К</td><td>Bottom</td><td>2</td><td>0.035</td><td>0.024</td><td>-</td><td>0.024</td></td<>	n261	К	Bottom	2	0.035	0.024	-	0.024
n260 J Back 2 1.000 0.741 0.429 0.741 n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 0.027 <t< td=""><td>n261</td><td>К</td><td>Right</td><td>2</td><td>1.000</td><td>0.676</td><td>0.301</td><td>0.676</td></t<>	n261	К	Right	2	1.000	0.676	0.301	0.676
n260 J Front 2 0.032 0.023 0.093 0.093 n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n261	К	Left	2	0.049	0.033	-	0.033
n260 J Top 2 0.192 0.142 - 0.142 n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Back	2	1.000	0.741	0.429	0.741
n260 J Bottom 2 0.108 0.080 - 0.080 n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Front	2	0.032	0.023	0.093	0.093
n260 J Right 2 0.093 0.069 - 0.069 n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Тор	2	0.192	0.142	-	0.142
n260 J Left 2 0.672 0.498 0.217 0.498 n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Bottom	2	0.108	0.080	-	0.080
n260 K Back 2 1.000 0.676 0.254 0.676 n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Right	2	0.093	0.069	=	0.069
n260 K Front 2 0.230 0.155 0.228 0.228 n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	J	Left	2	0.672	0.498	0.217	0.498
n260 K Top 2 0.537 0.363 0.201 0.363 n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	К	Back	2	1.000	0.676	0.254	0.676
n260 K Bottom 2 0.027 0.019 - 0.019 n260 K Right 2 1.000 0.676 0.231 0.676	n260	K	Front	2	0.230	0.155	0.228	0.228
n260 K Right 2 1.000 0.676 0.231 0.676	n260	K	Тор	2	0.537	0.363	0.201	0.363
	n260	К	Bottom	2	0.027	0.019	-	0.019
n260 K Left 2 0.023 0.015 - 0.015	n260	K	Right	2	1.000	0.676 C		0.676
	n260	K	Left	2	0.023	0.015	-	0.015

Note: Adjusted factor is (simulated PD on desired exposure plane)/(PD on worst-surface at 2mm evaluation distance) out of all beams and out of all channels. See Power Density Simulation Report.

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Table C-2 5G mmW NR FR2 psPD - Open

			00 111111111	I IXZ PSI D -	Open		
NR Band	<u>Antenna</u>	<u>Surface</u>	Evaluation Distance (mm)	Adjustment Factor due to Simulation	Adjusted Reported psPD (mW/cm²)	Measured Total psPD (mW/cm²)	Final Reported psPD (mW/cm²)
n258	J	Back	2	1.000	0.741	0.447	0.741
n258	J	Front	2	0.032	0.024	0.003	0.024
n258	J	Тор	2	0.130	0.096	-	0.096
n258	J	Bottom	2	0.129	0.096	-	0.096
n258	J	Right	2	0.122	0.090	-	0.090
n258	J	Left	2	0.134	0.099	-	0.099
n258	K	Back	2	1.000	0.676	0.339	0.676
n258	K	Front	2	0.723	0.489	0.046	0.489
n258	K	Тор	2	0.413	0.279	0.263	0.279
n258	K	Bottom	2	0.037	0.025	-	0.025
n258	K	Right	2	1.000	0.676	0.333	0.676
n258	K	Left	2	0.016	0.010	-	0.010
n261	J	Back	2	1.000	0.759	0.599	0.759
n261	J	Front	2	0.025	0.019	0.004	0.019
n261	J	Тор	2	0.105	0.080	-	0.080
n261	J	Bottom	2	0.036	0.028	-	0.028
n261	J	Right	2	0.058	0.044	-	0.044
n261	J	Left	2	0.092	0.070	-	0.070
n261	K	Back	2	1.000	0.676	0.187	0.676
n261	K	Front	2	0.826	0.558	0.215	0.558
n261	K	Тор	2	0.422	0.285	0.230	0.285
n261	K	Bottom	2	0.031	0.021	-	0.021
n261	K	Right	2	1.000	0.676	0.321	0.676
n261	K	Left	2	0.015	0.010	-	0.010
n260	J	Back	2	1.000	0.741	0.448	0.741
n260	J	Front	2	0.046	0.034	0.003	0.034
n260	J	Тор	2	0.190	0.141	-	0.141
n260	J	Bottom	2	0.109	0.081	-	0.081
n260	J	Right	2	0.094	0.070	-	0.070
n260	J	Left	2	0.082	0.061	-	0.061
n260	K	Back	2	0.968	0.654	0.285	0.654
n260	K	Front	2	0.649	0.439	0.198	0.439
n260	K	Тор	2	0.535	0.362	0.176	0.362
n260	K	Bottom	2	0.027	0.018 -		0.018
n260	K	Right	2	1.000	0.676	0.272	0.676
n260	K	Left	2	0.016	0.011	-	0.011

Note: Adjusted factor is (simulated PD on desired exposure plane)/(PD on worst-surface at 2mm evaluation distance) out of all beams and out of all channels. See Power Density Simulation Report.

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The TER results listed in the tables below may slightly differ from the numerical sum of each individual transmitter due to significant digit rounding in the calculations.

Table C-3
5G mmW NR FR2 Head Total Exposure Ratio

		NR FR2	Ant 2	MIMO	1	2	5 GHz WLAN MIMO Reported SAR	MIMO	NR FR2 + 2.4 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1	NR FR2 + Bluetooth Ant 2	NR FR2 +5 GHz WLAN MIMO	NR FR2 + 6 GHz WLAN MIMO		NR FR2 + Bluetooth Ant 1 + 5 GHz WLAN MIMO			NR FR2 + Bluetooth	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2 + 5 GHz WLAN MIMO	Ant 1 + 2.4 GHz	NR FR2 + 2.4 GHz WLAN MIMO + 5	NR FR2 + 2.4 GHz WLAN MIMO + 6 GHz WLAN MIMO
			12.0 dBm	15.0 dBm	10.5 dBm	8.5 dBm	14.0 dBm	13.0 dBm											WOOD INCOME.	WEAR MINIO		1
		mW/cm²	W/kg	W/kg	W/kg	W/kg	W/Ng	W/kg														
		1	2	3	4	5	7	,	1+3	1+4	1+5	1+7	1+9	1+4+2	1+4+7	1+5+7	1+4+9	1+5+9	1+4+2+7	1+4+2+9	1+3+7	1+3+9
A	Applicable Limit	1.0	1.6	1.6	1.6	1.6	1.6	1.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Front Side	Reported Value	0.390	0.003	0.365	0.305	0.000	0.314	0.368														
FIGUR 2000	Ratio to Limit	0.390	0.002	0.228	0.191	0.000	0.196	0.230	0.618	0.581	0.390	0.586	0.620	0.583	0.777	0.586	0.811	0.620	0.779	0.813	0.814	0.848

Table C-4
5G mmW NR FR2 Body-Worn Total Exposure Ratio

						•••			—		,		J	-2.6								
		NR FR2	Ant 2	MIMO	1	2	5 GHz WLAN MIMO Reported SAR	MIMO	NR FR2 + 2.4 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1	NR FR2 + Bluetooth Ant 2	NR FR2 + 5 GHz WLAN MIMO	NR FR2 +6 GHz WLAN MIMO		NR FR2 + Bluetooth Ant 1 + 5 GHz WLAN MIMO			NR FR2 + Bluetooth	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2 + 5 GHz WLAN MIMO	Ant 1 + 2.4 GHz	NR FR2 + 2.4 GHz	WLAN MIMO + 6
			18.0 dBm	21.0 dBm	18.5 dBm	15.0 dBm	20.0 dBm	13.0 dBm											WOOD WIND	WEAR MINE		1 1
		mW/cm*	W/kg	W/kg	W/kg	W/kg	W/kg	W/kg														1 1
		1	2	3	4	5	7	9	1+3	1+4	1+5	1+7	1+9	1+4+2	1+4+7	1+5+7	1+4+9	1+5+9	1+4+2+7	1+4+2+9	1+3+7	1+3+9
	Applicable Limit	1.0	1.6	1.6	1.6	1.6	1.6	1.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Back Side	Reported Value	0.759	0.015	0.032	0.037	0.007	0.022	0.012														
Mark Japan	Ratio to Limit	0.759	0.009	0.020	0.023	0.004	0.014	0.008	0.779	0.782	0.763	0.773	0.767	0.792	0.796	0.777	0.790	0.771	0.805	0.799	0.793	0.787

Table C-5
5G mmW NR FR2 Hotspot Total Exposure Ratio

		NR FR2	2.4 GHz WLAN Ant 2 Reported SAR	MIMO Reported SAR	.,	2 Reported SAR	5 GHz WLAN MIMO Reported SAR	NR FR2 + 2.4 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1	NR FR2 + Bluetooth Ant 2	NR FR2 +5 GHz WLAN MIMO		NR FR2 + Bluetooth Ant 1 + 5 GHz WLAN MIMO	NR FR2 + Bluetooth	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2 + 5 GHz WLAN MIMO	NR FR2 + 2.4 GHz
		mW/cm²	18.0 dBm W/kg	21.0 dBm W/kg	18.5 dBm W/kg	15.0 dBm W/kg	20.0 dBm W/kg									
		1	2	3	4	5	7	1+3	1+4	1+5	1+7	1+4+2	1+4+7	1+5+7	1+4+2+7	1+3+7
,	Applicable Limit	1.0	1.6	1.6	1.6	1.6	1.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Back Side	Reported Value	0.759	0.026	0.052	0.059	0.008	0.047		•			•				
Back Side	Ratio to Limit	0.759	0.016	0.033	0.037	0.005	0.029	0.792	0.796	0.764	0.788	0.812	0.825	0.793	0.842	0.821
Front Side	Reported Value	0.390	0.086	0.286	0.245	0.033	0.105									
Front side	Ratio to Limit	0.390	0.054	0.179	0.153	0.021	0.066	0.569	0.543	0.411	0.456	0.597	0.609	0.476	0.663	0.634
Top Edge	Reported Value	0.363	0.000	0.348	0.284	0.000	0.162									
Top Eage	Ratio to Limit	0.363	0.000	0.218	0.178	0.000	0.101	0.581	0.541	0.363	0.464	0.541	0.642	0.464	0.642	0.682
Bottom Edge	Reported Value	0.084	0.139	0.118	0.000	0.072	0.078									
BOLLOITEURE	Ratio to Limit	0.084	0.087	0.074	0.000	0.045	0.049	0.158	0.084	0.129	0.133	0.171	0.133	0.178	0.220	0.207
Right Edge	Reported Value	0.676	0.000	0.000	0.000	0.000	0.000									
rogin Euge	Ratio to Limit	0.676	0.000	0.000	0.000	0.000	0.000	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676
Left Edge	Reported Value	0.549	0.045	0.118	0.089	0.015	0.035									
Leit Eage	Ratio to Limit	0.549	0.028	0.074	0.056	0.009	0.022	0.623	0.605	0.558	0.571	0.633	0.627	0.580	0.655	0.645

Table C-6
5G mmW NR FR2 Phablet Total Exposure Ratio

	30 111111111111111111111111111111111111	\ I I\Z I II	abict 10to	ii Exposui	Citatio	
		NR FR2	5 GHz WLAN MIMO Reported SAR	6 GHz WLAN MIMO Reported SAR	NR FR2 + 5 GHz WLAN MIMO	NR FR2 + 6 GHz WLAN MIMO
		mW/cm²	W/kg	W/kg		
		1	3	5 VV/Ng	1+3	1+5
App	olicable Limit	1.0	4.0	4.0	1.0	1.0
De el Cide	Reported Value	0.759	0.083	0.021		
Back Side	Ratio to Limit	0.759	0.021	0.005	0.780	0.764
Format Circle	Reported Value	0.390	0.925	0.267		,
Front Side	Ratio to Limit	0.390	0.231	0.067	0.621	0.457
Tan Edan	Reported Value	0.363	1.539	0.309		
Top Edge	Ratio to Limit	0.363	0.385	0.077	0.748	0.440
Datter Edea	Reported Value	0.084	1.275	0.247		,
Bottom Edge	Ratio to Limit	0.084	0.319	0.062	0.403	0.146
Dight Edgo	Reported Value	0.676	0.000	0.000		
Right Edge	Ratio to Limit	0.676	0.000	0.000	0.676	0.676
Left Edge	Reported Value	0.549	0.095	0.033		
Lett Edge	Ratio to Limit	0.549	0.024	0.008	0.573	0.557

	Worst Case Phablet TER	Worst Case NFC Reported SAR	Worst Case UWB Reported SAR	Phablet Worst Case Scenario + NFC + UWB
		W/kg	W/kg	
Applicable Limit	1.0	4.0	4.0	1.0
Reported Value		0.009	0.002	
Ratio to Limit	0.780	0.002	0.001	0.783

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Table C-7 5G mmW NR FR2 UMPC Body Total Exposure Ratio

										•							_					
		NR FR2	Ant 2	2.4 GHz WLAN MIMO Reported SAR	1	2	MIMO	6 GHz WLAN MIMO Reported SAR	NR FR2 + 2.4 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1	NR FR2 + Bluetooth Ant 2	NR FR2 + 5 GHz WLAN MIMO	NR FR2 + 6 GHz WLAN MIMO		NR FR2 + Bluetooth Ant 1 + 5 GHz WLAN MIMO			NR FR2 + Bluetooth	Ant 1 + 2.4 GHz	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2 + 6 GHz WLAN MIMO	NR FR2 + 2.4 GHz WLAN MIMO + 5 GHz WLAN MIMO	WLAN MIMO + 6
			14.0 dBm	17.0 d8m	14.0 dBm	15.0 dBm	20.0 dBm	13.0 dBm	I										W.C. W. W. W.	WEAR MINIO	1 .	1
		ntW/cm*	W/kg	W/kg	W/kg	W/kg	W/kg	W/kg														1
		1	2	3	4	5	7	,	1+3	1+4	1+5	1+7	1+9	1+4+2	1+4+7	1+5+7	1+4+9	1+5+9	1+4+2+7	1+4+2+9	1+3+7	1+3+9
	Applicable Limit	1.0	1.6	1.6	1.6	1.6	1.6	1.6	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Back Side	Reported Value	0.759	0.066	0.082	0.091	0.194	0.132	0.029														
Back Sibil	Ratio to Limit	0.759	0.041	0.051	0.057	0.121	0.083	0.018	0.810	0.816	0.880	0.842	0.777	0.857	0.898	0.963	0.834	0.898	0.940	0.875	0.893	0.828
Front Side	Reported Value	0.558	0.075	0.068	0.098	0.058	0.145	0.043														
Front Sibil	Ratio to Limit	0.558	0.047	0.043	0.061	0.036	0.091	0.027	0.601	0.619	0.594	0.649	0.585	0.666	0.710	0.685	0.646	0.621	0.757	0.693	0.691	0.627
Top Edee	Reported Value	0.362	0.000	0.121	0.112	0.000	0.263	0.063														
TOPLOGE	Ratio to Limit	0.362	0.000	0.076	0.070	0.000	0.164	0.039	0.438	0.432	0.362	0.526	0.401	0.432	0.596	0.526	0.471	0.401	0.596	0.471	0.602	0.477
Bottom Edee	Reported Value	0.096	0.087	0.115	0.000	0.117	0.223	0.029														
agttom Edge	Ratio to Limit	0.096	0.054	0.072	0.000	0.073	0.139	0.018	0.168	0.096	0.169	0.235	0.114	0.150	0.235	0.309	0.114	0.187	0.290	0.169	0.307	0.186
Right Edge	Reported Value	0.676	0.000	0.000	0.000	0.000	0.000	0.000														
sugnit cage	Ratio to Limit	0.676	0.000	0.000	0.000	0.000	0.000	0.000	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676
	Reported Value	0.099	0.000	0.000	0.000	0.000	0.000	0.000														
Left Edge	Ratio to Limit	0.099	0.000	0.000	0.000	0.000	0.000	0.000	0.099	0.099	0.099	0.099	0.029	0.099	0.099	0.099	0.099	0.029	0.099	0.099	0.099	0.099

Table C-8

5G mmW NR FR2 UMPC Extremity Total Exposure Ratio

		NR FR2	Ant 2	2.4 GHz WLAN MIMO Reported SAR	1	2	MIMO	6 GHz WLAN MIMO Reported SAR	NR FR2 + 2.4 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1	NR FR2 + Bluetooth Ant 2	NR FR2 + 5 GHz WLAN MIMO	NR FR2 + 6 GHz WLAN MIMO	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2				NR FR2 + Bluetooth	NR FR2 + Bluetooth Ant 1 + 2.4 GHz WLAN Ant 2 + 5 GHz WLAN MIMO	Ant 1 + 2.4 GHz	WLAN MIMO + 5	NR FR2 + 2.4 GHz WLAN MIMO + 6 GHz WLAN MIMO
			14.0 dBm	17.0 dBm	14.0 dBm	12.0 dBm	17.0 dBm	13.0 dBm													1	
		mW/cm*	W/kg	W/kg	W/kg	W/kg	W/kg	W/kg														زــــــــــــــــــــــــــــــــــــــ
		1	2	3	4	5	7	,	1+3	1+4	1+5	1+7	1+9	1+4+2	1+4+7	1+5+7	1+4+9	1+5+9	1+4+2+7	1+4+2+9	1+3+7	1+3+9
	Applicable Limit	1.0	4.0	4.0	4.0	4.0	4.0	4.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Back Side	Reported Value	0.759	0.216	0.362	0.278	0.113	0.366	0.220														
Back Sibil	Ratio to Limit	0.759	0.054	0.091	0.070	0.028	0.092	0.055	0.850	0.829	0.787	0.851	0.814	0.883	0.920	0.879	0.884	0.842	0.974	0.938	0.941	0.905
Front Side	Reported Value	0.558	0.208	0.326	0.285	0.107	0.381	0.211														
Front Side	Ratio to Limit	0.558	0.052	0.082	0.071	0.027	0.095	0.053	0.640	0.629	0.585	0.653	0.611	0.681	0.725	0.680	0.682	0.638	0.777	0.734	0.735	0.692
Top Edee	Reported Value	0.362	0.000	0.428	0.382	000.0	0.624	0.315														
roproge	Ratio to Limit	0.362	0.000	0.107	0.096	000.0	0.156	0.079	0.469	0.458	0.362	0.518	0.441	0.458	0.614	0.518	0.536	0.441	0.614	0.536	0.625	0.548
Bottom Edee	Reported Value	0.096	0.214	0.398	0.000	0.114	0.534	0.235														
ao ttorri cage	Ratio to Limit	0.096	0.054	0.100	0.000	0.029	0.134	0.059	0.196	0.096	0.125	0.230	0.155	0.150	0.230	0.258	0.155	0.183	0.283	0.208	0.329	0.254
Right Edge	Reported Value	0.676	0.000	0.000	0.000	0.000	0.000	0.000														
~grit Edge	Ratio to Limit	0.676	0.000	0.000	0.000	0.000	0.000	0.000	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676	0.676
Left Edge	Reported Value	0.099	0.000	0.000	0.000	0.000	0.000	0.000														
Cent code	Ratio to Limit	0.099	0.000	0.000	0.000	0.000	0.000	0.000	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099	0.099

	Worst Case UMPC Extremity TER	Worst Case NFC Reported SAR	Worst Case UWB Reported SAR	NR FR2 + 2.4 GHz WLAN MIMO
		W/kg	W/kg	
	1	2	3	1+3
Applicable Limit	1.0	4.0	4.0	1.0
Reported Value		0.010	0.000	
Ratio to Limit	0.974	0.003	0.000	0.977

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Notes:

- 1. Worst-case power density results for each test configuration among all antenna arrays and among all supported bands were considered for TER analysis.
- 2. If test positions were not required to be evaluated for WLAN SAR per FCC KDB publication 248227, the worst-case WLAN SAR result for the applicable exposure conditions was used for simultaneous transmission analysis. Any such values are indicated in the above tables in blue.
- 3. If Part 1 SAR report does not include standalone WLAN MIMO results, then per KDB Publication 248227 D01v02r02, SAR for MIMO was evaluated by following the simultaneous SAR provisions from KDB Publication 447498 D01v06 by evaluating the sum of the 1g SAR values of each antenna transmitting independently. Any such values are indicated in the above tables in green.
- 4. When additional sides were tested at a distance greater than 2mm for hotspot and body-worn configurations, those power density results were used for TER. Otherwise, power density results at 2mm were considered as a more conservative evaluation.
- Per FCC guidance, the bands/modes that are not required to be evaluated for Phablet SAR are not considered for TER analysis.
- 6. Per FCC guidance, for power density measurements, a test separation distance of 2 mm was used for phablet configuration due to probe restraints.
- 7. Worst-case front side reported psPD was considered for Head TER analysis.
- 8. The worst-case between Adjusted Reported_psPD and Measured Total psPD was chosen for TER analysis. The bolded psPD values in Table C-1 and Table C-2 indicate the worst-case Reported psPD used in TER analysis.
- In WLAN MIMO operations, each antenna transmits at target powers to achieve the MIMO target powers as indicated above.
- 10. 4G LTE terms in the introduction and equation derivation equally apply to NR FR1.

The above numerical summed PD and SAR for all the worst-case simultaneous transmission conditions were below the Total Exposure Ratio. Therefore, the above analysis is sufficient to determine no further test cases are required and that simultaneous transmission is compliant to the FCC RF Exposure Limit.

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Mathematical Derivation of TER Compliance

Total Normalized RFx = Normalized RFx
$$_{Time\ Averaged\ WWAN}$$
 + Normalized RFx $_{WLAN}$ ≤ 1.0 (1)

Since WWAN Smart Transmit algorithm adds directly the time-averaged RF exposure from 4G and time-averaged RF exposure from 5G mmW NR, per chipset manufacturer's guidance, Normalized RF exposure from 4G and from 5G mmW NR could be assumed as

Normalized RFx _{Time Averaged WWAN} =
$$\frac{4G SAR}{4G SAR Limit} + \frac{5G mmW NR psPD}{5G mmW NR psPD Limit} \le 1.0$$
 (2)

Smart Transmit algorithm assumes that 4G and 5G mmW NR hotspots are co-located and therefore:

Time Averaged WWAN =
$$[x(t) \times A] + [(1-x(t)) \times B] \le 1.0$$
 Normalized Limit (3)

A = Max normalized time-averaged SAR exposure from 4G

B = Max normalized time-averaged PD exposure from 5G mmW NR

x(t) = Ranges between [0,1]

 $x(t) \times A = Percentage of normalized time-averaged RF exposure from 4G$

 $(1-x(t)) \times B = Remaining percentage of RF exposure contribution from 5G mmW NR$

Smart Transmit controls "x" in real time such that the sum of these exposures never exceeds 1.0 Normalized Limit. If the equations below (4a, 4b) are proven, then, mathematically equation (5) would be proven.

$$A + norm. SAR from WLAN \le 1.0 normalized limit$$
 (4a)

$$B + norm. SAR from WLAN \le 1.0 normalized limit$$
 (4b)

$$[x(t) \times A] + [(1-x(t)) \times B] + norm. SAR from WLAN \le 1.0 normalized limit$$
 (5)

Without 5G mmW NR, Smart Transmit limits the maximum RF exposure contributed from 4G to 100% normalized exposure. For this device, the manufacturer has added an additional permanent back-off (indicated below as WWAN backoff) for every beam in the calculations for input power.limits used in the EFS file. Therefore.

Smart Tx WWAN:
$$A = max$$
 (normalized SAR exposure from $4G$) ≤ 1.0 normalized limit (6a) Smart Tx WWAN: $B = max$ (normalized PD exposure from $5G$ mmW NR) $x10^{(-WWAN)}$ backoff in dB)/ $10 \leq 1.0$ normalized limit (6b)

To demonstrate simultaneous transmission compliance in equation (1), below equations (7a & 7b) obtained by combining equations (4a & 4b) and (6a & 6b), should be proven for simultaneous transmission compliance:

Total Normalized RFx = Normalized SAR
$$_{4G\ WWAN}$$
 + Normalized SAR $_{WLAN}$ < 1.0 (7a)
Total Normalized RFx = $10^{(-WWAN\ backoff\ in\ dB)/10}x$ Normalized psPD $_{5G\ mmW\ NR\ WWAN}$ +

Fotal Normalized RFx =
$$10^{(-WWAN \ backoff \ in \ aB)/10}x$$
 Normalized psPD $_{5G\ mmW\ NR\ WWAN}$ +

Normalized SAR $_{WLAN}$ < 1.0 (7b)

which are re-written as:

Total Normalized RFx =
$$\frac{4G \, SAR}{4G \, SAR \, Limit} + \frac{WLAN \, SAR}{WLAN \, SAR \, Limit} < 1$$
 (8a)

$$Total\ Normalized\ RFx\ =\ 10^{(-WWAN\ backoff\ in\ dB)/10}*\frac{5G\ mmW\ NR\ psPD}{5G\ mmW\ NR\ psPD\ Limit} + \frac{WLAN\ SAR}{WLAN\ SAR\ Limit} < 1 \tag{8b}$$

Analysis for equation (8a) is performed in Appendix D of FCC SAR Evaluation Report (Part 1). Analysis for equation (8b) is performed in this appendix.

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